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## On the activity and stability of Pt-K/Al<sub>2</sub>O<sub>3</sub> LNT catalysts for diesel soot and NO<sub>x</sub> abatement



R. Matarrese<sup>a</sup>, L. Castoldi<sup>a</sup>, N. Artioli<sup>a</sup>, E. Finocchio<sup>b</sup>, G. Busca<sup>b</sup>, L. Lietti<sup>a,\*</sup>

- <sup>a</sup> Dipartimento di Energia, Laboratory of Catalysis and Catalytic Processes and NEMAS, Centre of Excellence, Politecnico di Milano, P.zza L. da Vinci 32, Milano, Italy
- <sup>b</sup> Laboratorio di Chimica delle Superfici e Catalisi Industriale, Dipartimento di Ingegneria Civile, Chimica ed Ambientale, Università di Genova, Piazzale Kennedy 1, I-16129 Genova, Italy

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#### ABSTRACT

DPNR Pt-K/Al<sub>2</sub>O<sub>3</sub> catalyst has been studied for the simultaneous removal of soot and NO<sub>x</sub>, in the presence of both water and carbon dioxide. In particular, the effect of soot on the NO<sub>x</sub> storage activity and on the stability of Pt-K/Al<sub>2</sub>O<sub>3</sub> catalyst has been addressed. It has been found that: (i) the presence of soot decreases the NO<sub>x</sub> storage activity at any temperature in the range 250–350 °C; (ii) the stability of the adsorbed species is lower in the presence of soot; (iii) nitrates ad-species directly interact with soot and participate to the soot combustion; (iv) aged catalyst shows a lower storage capacity and a lower soot oxidation activity attributed to loss of K-active species.

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#### 1. Introduction

The main pollutants emitted by diesel engines are nitrogen oxides and soot particles (particulate matter, PM) whose adverse effects on the environment and human health are widely recognized. For this reason, the abatement of  $NO_x$  and particulate from diesel exhausts is a major issue nowadays, forced by the application of the upcoming legislative emissions standards. In fact, diesel particulate filters (DPF) are typically used to cope with the PM emission standards required by the current legislation. Concerning  $NO_x$  reduction, the existing technical solutions are primarily based on the technological improvement of the diesel engines (e.g. by means of advanced fuel injection technologies, exhaust gas recirculation (EGR) control, etc.). However it is widely accepted that in order to meet the upcoming legislative emissions standards (e.g. Euro VI (2014) regulations, in Europe), the adoption of after-treatment systems will be required [1,2].

The three-way technology, currently used on the traditional stoichiometric gasoline-powered engines, is unable to reduce  $NO_X$  under the typical lean conditions of diesel engines. Accordingly innovative  $NO_X$  abatement technologies have been developed. Among them the  $NH_3$ /urea selective catalytic reduction (SCR) and the  $NO_X$  storage-reduction (NSR), also quoted as lean  $NO_X$  trap

(LNT), are widely accepted as the most promising  $NO_x$  control strategies. The former has been essentially developed for heavyduty vehicles while for the light vehicles a competition between SCR and NSR, still exists [3]. In this complex technological context, the development of integrated De-NO<sub>x</sub> and De-soot after-treatment technologies have also been proposed. One example is the diesel clean advanced technology (D-CAT) emission control system proposed by the Toyota group and recently equipped on its Avensis model [4]. The heart of the D-CAT system is the DPNR (diesel PM and NO<sub>x</sub> reduction) system which has the unique capacity to remove simultaneously both soot and NO<sub>x</sub> via the combination of a ceramic wall-flow filter coated with a new catalytic layer [5,6]. The DPNR catalyst is very similar to that already proposed by Toyota for its lean NO<sub>x</sub> traps (LNT catalysts), initially designed for use with Toyota's lean-burn gasoline engines [7] and is composed of a high surface area support material (often  $\gamma$ -alumina), precious metals (usually a combination of Pt and Rh) and a basic component, such as Ba or K phases, which acts as NO<sub>x</sub> storage material. As the LNTs, DPNR systems work under cyclic conditions alternating long lean periods with short regeneration periods under rich conditions [5,6]. During the lean phase the NO<sub>x</sub> produced by the engine are oxidized and adsorbed on the alkaline or alkaline-earth metal oxide component; during the rich phase the stored NO<sub>x</sub> species are reduced to molecular nitrogen by CO, H<sub>2</sub> and UHCs. In addition, under lean conditions the DPNR system works as a catalyzed soot filter (CSF) in which soot combustion is primarily ascribed to NO2 formed upon NO oxidation over noble metals, followed by NO recycle to NO<sub>2</sub>

<sup>\*</sup> Corresponding author. Tel.: +39 02 2399 3272, fax: +39 02 7063 8173. E-mail address: luca.lietti@polimi.it (L. Lietti).

as suggested by Krishna et al. [8]. Moreover, also the  $NO_x$  storage function of the LNT catalysts is claimed to assist the combustion of soot by means of the  $NO_x$  adsorbed species [6]. Of note, Toyota researchers proposed that active oxygen species, which are formed during  $NO_x$  adsorption, are effective in soot oxidation under rich conditions as well [5,6].

In spite of the fact that many studies are available in the literature concerning the behaviour of LNT systems in the removal of  $NO_X$  (e.g. the reviews by Epling et al. [9] or Roy and Baiker [10] and references therein), investigations on the DPNR system are very scarce. Besides, most of them are focused on the effect of soot on the  $NO_X$  storage efficiency of LNT systems or on the interaction between the  $NO_X$  storage function and soot oxidation capacity [8,11–14] rather than on the combined soot- $NO_X$  reduction activity under lean-rich cycling conditions, typical of the DPNR technology [15].

In a previous work from our group [16] the capability of a model PtBa/Al<sub>2</sub>O<sub>3</sub> LNT catalyst to remove simultaneously soot and NO<sub>x</sub> according to DPNR concept has been addressed. It has been shown that during the lean phase NO<sub>x</sub> are stored on the catalyst surface, while soot oxidation simultaneously occurs involving NO<sub>2</sub> formed upon NO oxidation over Pt sites. However a role of the  $NO_x$  adsorbed species in the soot oxidation has also been invoked [17,18]. The reactivity of a model Pt-K/Al<sub>2</sub>O<sub>3</sub> catalyst has been recently investigated and compared with an analogous Pt-Ba/Al<sub>2</sub>O<sub>3</sub> sample [19,20]. It has been found that the two samples have similar De-NO<sub>x</sub> activity but the K-containing system shows significantly higher activity for soot combustion. According to the literature [21-23] it has been suggested that potassium may favour soot oxidation through the formation of low melting point compounds, thus improving the mobility of the active surface species and consequently improving activity according to a higher contact between catalysts and soot. However, because of alkali mobility, K-based catalysts are blamed for low thermal stability which is associated to several technological problems such as interactions with the monolith support or loss of active phase (i.e. with consequent catalysts deactivation) due to volatilization and/or dissolution by condensed

On these bases, in this work the reactivity of a model Pt-K/Al $_2$ O $_3$  catalyst has been investigated in the simultaneous removal of NO $_x$  and soot under more realistic conditions (i.e. in the presence of CO $_2$  and H $_2$ O and in the temperature range 250–350 °C) by performing isothermal concentration step change (ICSC) experiments. The same experiments have been performed in the absence of soot in order to analyze the influence of soot on the behaviour of the LNT catalyst in terms of NO $_x$  storage–reduction. Also a comparison with a model Pt-Ba/Al $_2$ O $_3$  catalyst is provided to obtain information on the interaction between De-NO $_x$  and De-soot performances and on the role of the storage component (i.e. K vs. Ba). Moreover, the activity and stability of the Pt-K/Al $_2$ O $_3$  catalysts during repeated lean-rich cycles in the presence of soot have been also investigated. FT-IR spectroscopy has also been used to compare the peculiarities of the fresh and aged Pt-K/Al $_2$ O $_3$  sample.

#### 2. Experimental

#### 2.1. Catalysts preparation and characterization

A homemade Pt-K/Al<sub>2</sub>O<sub>3</sub> (nominal loadings 1/5.4/100 w/w) catalyst has been prepared by incipient wetness impregnation of a commercial alumina sample (Versal 250 from UOP) with an aqueous solution of dinitro-diammine platinum (Strem Chemicals, 5% Pt in ammonium hydroxide) and subsequently with a solution of potassium acetate (Aldrich, 99%). The powder has been dried at 80 °C and calcined in air at 500 °C for 5 h after each impregnation step. The impregnation order (first Pt and then K) has

been selected in order to ensure a good dispersion and stability of the noble metal and of the alkali component on the alumina support, in line with recipes of Toyota patents [7]. This sample has molar amount of K comparable to that contained in the Pt-Ba/Al<sub>2</sub>O<sub>3</sub> (1/20/100 w/w) model catalyst previously used for similar studies (0.146 mol K or Ba/100 g of Al<sub>2</sub>O<sub>3</sub>) and reported here for comparisons [17,18]. The catalyst was characterized by XRD analysis (Brüker D8 Advanced Instrument equipped with graphite monochromator on the diffracted beam), surface area and pore size distribution by N<sub>2</sub> adsorption–desorption at 77 K (Micromeritics TriStar 3000 instrument) and Pt dispersion by hydrogen pulse chemisorption at 0 °C (TPD/R/O 1100 Thermo Fischer Instrument). The Pt-K/Al<sub>2</sub>O<sub>3</sub> sample presents a surface area near 167 m²/g<sub>cat</sub> and pore volume of 0.90 cm³/g<sub>cat</sub>, while the Pt dispersion is close to 30%.

Both fresh and aged Pt- $K/Al_2O_3$  catalysts were analyzed by SEM-EDS technique to evaluate the potassium content; loadings of 6.2% and 5.7% have been estimated in the fresh and in the aged samples, respectively. Printex U (Evonik-Degussa) was used as model soot, which is widely used as a model substance for diesel particulate [8,15,24] and whose properties are well described in the literature [25,26].

Catalyst-soot mixtures were prepared by gently mixing in a vial the catalyst powder with soot (9:1 catalyst/soot ratio), thus realizing a loose contact.

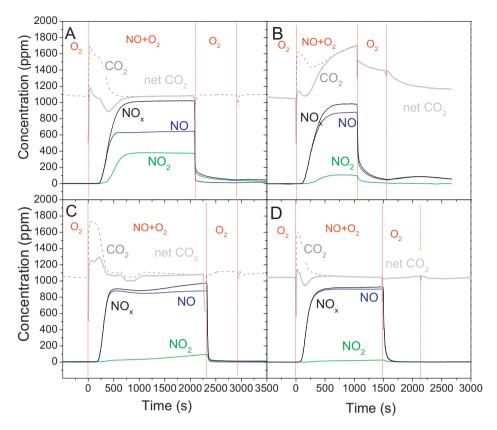
Further details of catalyst preparation and characterization are reported elsewhere [27,28].

#### 2.2. Catalytic tests

All reactivity tests were performed in a micro flow-reactor apparatus consisting of a quartz tube reactor (7 mm i.d.) connected to a mass spectrometer (Omnistar 200, Pfeiffer Vacuum), a micro-GC (Agilent 3000A) and an UV analyzer (Limas 11HW, ABB) for the on-line analysis of the outlet gases (NO, NO<sub>2</sub>, N<sub>2</sub>, H<sub>2</sub>, O<sub>2</sub>, CO, CO<sub>2</sub>, N<sub>2</sub>O and NH<sub>3</sub>). 66 mg of the soot-catalyst mixture (corresponding to 59.4 mg of the bare catalyst and 6.6 mg of soot) was used in each run. Prior catalytic activity runs, the catalyst sample has been conditioned by performing few storage/regeneration cycles. For this purpose, isothermal concentration step change (ICSC) experiments have been performed at 350 °C by imposing a rectangular step feed of NO (1000 ppm)+3% v/v O<sub>2</sub> in flowing He + 1% H<sub>2</sub>O + 0.1% CO<sub>2</sub> (lean phase) until catalyst saturation. Then the NO and O<sub>2</sub> concentrations have been stepwise decreased to zero, and a He purge at the same temperature (350 °C) has been performed. This leads to the desorption of weakly adsorbed  $NO_x$  species. After the He purge, catalyst regeneration (rich phase) has been carried out with  $H_2$  (3500 ppm) in flowing He + 1% H<sub>2</sub>O + 0.1% CO<sub>2</sub>. Conditioning lasted until a reproducible behaviour was obtained; this typically required 3-4 adsorption-reduction cycles.

After catalyst conditioning at 350 °C, the catalytic activity of Pt-K/Al $_2$ O $_3$  has been tested with typical ICSC runs in the temperature range 250–350 °C. Part of the conditioned catalyst has been also mixed with soot (9:1 w/w ratio) and ICSC run have been performed on catalyst/soot mixture at the same temperatures.

Finally, the stability of the Pt-K/Al $_2O_3$  catalyst has also been studied. The pre-conditioned catalyst has been mixed with soot (9:1 w/w ratio) and ICSC experiment has been performed at 350 °C. During this first run (Run 1), soot has been progressively consumed. After the complete consumption of soot, the clean sample has been mixed again with soot (in the same ratio) (Run 2) and further lean-rich cycles at 350 °C have been carried out until the complete oxidation of particulate. The soot mixing and the catalyst cycling have been replicated another time (Run 3).



**Fig. 1.** Adsorption phase over Pt-K/Al $_2$ O $_3$  in the absence of soot (A: 350 °C; C: 250 °C) and in the presence of soot at different temperatures (B: 350 °C; D: 250 °C). 1000 ppm NO and 3% O $_2$  in the presence of H $_2$ O (1% v/v) and CO $_2$  (0.1% v/v).

#### 2.3. FT-IR analysis

The catalyst has been characterized by FT-IR spectroscopy upon CO and CO $_2$  adsorption. FT-IR analysis have been carried out by means of a Nicolet Nexus Fourier Transform instrument over both the fresh and aged Pt-K/Al $_2$ O $_3$  catalyst pressed in self supporting disks of average weight 30 mg. Catalysts have been outgassed at 350 °C before any adsorption experiment. After the activation step, CO adsorption has been carried out at liquid nitrogen temperature and the evolution of surface species has been studied after outgassing upon warming. CO $_2$  adsorption has been carried out at room temperature.

#### 3. Results and discussion

#### 3.1. Effect of temperature on the $NO_x$ storage-reduction activity

#### 3.1.1. $NO_x$ storage

The  $NO_x$  storage–reduction activity over Pt- $K/Al_2O_3$  catalyst in the absence of soot has been investigated in the 250–350 °C temperature range. The NO,  $NO_2$ ,  $NO_x$  (i.e.  $NO + NO_2$ ) and  $CO_2$  concentration profiles measured during the lean phase when 1000 ppm NO are fed to the reactor in the presence of  $O_2$ ,  $H_2O$  and  $CO_2$  are shown in Fig. 1. For the sake of brevity, only the data obtained at 250 °C and 350 °C are shown.

At  $350 \,^{\circ}$ C (Fig. 1A), upon NO admission to the reactor ( $t = 0 \, s$ ) a delay near 200 s is observed in the NO outlet concentration. Then, the NO concentration increases with time and reaches a steady state value near 645 ppm. NO<sub>2</sub> breakthrough is observed with a delay of 50 s with respect to NO and increases until its asymptotic level of

375 ppm. As well known, the NO<sub>2</sub> production is related to the NO oxidation on Pt sites (reaction (1)):

$$NO + 1/2O_2 \rightarrow NO_2$$
 (1)

The overall amount of  $NO_x$  stored at this temperature at the end of adsorption is near 0.56 mmol/ $g_{cat}$ , corresponding to the involvement of 40.5% of the overall K loading by assuming the formation of KNO $_3$  species. As shown in other works [27,28], both bidentate and ionic nitrates are present at this temperature at the end of the storage phase.

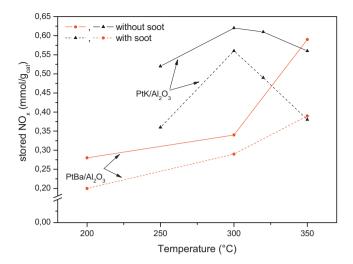
When the NO inlet concentration is switched off (t=2000 s), weakly adsorbed NO $_x$  species desorb [28], causing a decrement of roughly 25% in the amount of stored NO $_x$ .

Upon NO admission, an increase in the  $\mathrm{CO}_2$  concentration is also observed; this is due to the decomposition of surface carbonates upon  $\mathrm{NO}_x$  uptake according to the stoichiometry of the following reaction:

$$K_2CO_3 + 2NO + 3/2O_2 \rightarrow 2KNO_3 + CO_2$$
 (2)

In fact by subtracting from the  $CO_2$  concentration trace the amounts of  $CO_2$  evolved due to carbonate decomposition estimated according to the stoichiometry of reaction (2), we obtain a curve (net  $CO_2$  concentration trace reported in Fig. 1A) that roughly resembles the inlet  $CO_2$  concentration. In the experiments carried out in the presence of soot (see below), the net production of  $CO_2$  will be determined and this will be used to estimate the amounts of soot combusted.

The results of the  $NO_x$  adsorption carried out at the lowest investigated temperature are shown in Fig. 1C for comparison purpose. As apparent from Fig. 1A and C the  $NO_x$  storage behaviour of the catalyst is affected by the temperature: (i) the  $NO_x$  breakthrough



**Fig. 2.** Amounts of stored  $NO_x$  vs. temperature over  $Pt-K/Al_2O_3$  and  $Pt-Ba/Al_2O_3$  catalysts in the absence of soot (solid lines) and in the presence of soot (dotted lines)

increases from 90 s at 250 °C (Fig. 1C) to 200 s at 350 °C (Fig. 1A); (ii) the NO $_2$  concentration measured at the reactor outlet at the end of the NO $_2$  dose (i.e. at steady-state) increases with temperature as expected being the reaction kinetically controlled under our experimental conditions. Accordingly, the NO/NO $_2$  molar ratio calculated at the end of the storage phase decreases with temperature from 9.8 at 250 °C to 1.72 at 350 °C.

The quantitative analysis of the  $NO_x$  adsorption carried out at the various investigated temperatures is reported in Fig. 2 and Table 1. The amounts of  $NO_x$  stored up to steady state show a maximum near 0.6 mmol/ $g_{cat}$  at 300 °C, corresponding to the involvement of 45% of the overall K loading. These data have been compared with those collected over a Pt-Ba/Al<sub>2</sub>O<sub>3</sub> catalyst [17], as shown in Fig. 2 and Table 1. Over the Pt-Ba/Al<sub>2</sub>O<sub>3</sub> sample the storage capacity shows a distinct temperature dependence [29] with respect to Pt-K/Al<sub>2</sub>O<sub>3</sub>, in that it increases with temperature in the investigated T-range. However at 350 °C the storage capacity of the two catalysts is very similar. Worth to note that the fraction of K sites involved in the storage of  $NO_x$  (i.e. the K utilization) is higher than that of Ba at any temperature (i.e. 40.5% vs. 20.3%, respectively, at 350 °C).

In Table 1 the amounts of  $NO_x$  desorbed after NO shut-off (calculated in all cases 430 s after  $NO_x$  shut-off) are also reported. Over the Pt-K/Al<sub>2</sub>O<sub>3</sub> catalyst sample the amounts of desorbed  $NO_x$  increase with temperatures and are always higher than over Pt-Ba/Al<sub>2</sub>O<sub>3</sub> (12% vs. 8% at 350 °C).

#### 3.1.2. NO<sub>x</sub> reduction

The stored  $NO_x$  are then reduced under isothermal conditions by admitting  $H_2$  in the presence of  $H_2O$  and  $CO_2$  and results are shown in Fig. 3A (350 °C) and 3 C (250 °C).

At 350 °C (Fig. 3A), upon the addition of  $H_2$  (at t=0 s)  $N_2$  is immediately observed at the reactor outlet along with a  $CO_2$  consumption. This uptake of  $CO_2$  is in line with the occurrence of the overall reaction (3) which considers the re-adsorption of  $CO_2$  onto the K sites once  $NO_X$  have been reduced:

$$2KNO_3 + 5H_2 + CO_2 \rightarrow K_2CO_3 + N_2 + 5H_2O$$
 (3)

The  $\rm H_2$  consumption is initially nearly complete and after a delay near 200 s its concentration increases with time until the initial value of 3500 ppm. No production of ammonia or other byproducts like  $\rm N_2O$  is observed. Only a small amount of NO is detected along with nitrogen and this leads to a  $\rm N_2$  selectivity of ca. 95%. At the end

of the reduction phase (*t* = 300 s), the nitrates are all reduced and the catalytic surface is fully regenerated, as confirmed by N-balance.

Similar results have been obtained at the other investigated temperatures, i.e. 320, 300, 250 °C (see Fig. 3C at 250 °C): the main reduction product is nitrogen and only small amounts of NO are detected as byproduct. The overall nitrogen selectivity is in all cases higher than 95%. At all the investigated temperatures, the catalyst is fully regenerated at the end of the reduction phase, as pointed out from the N-balance.

#### 3.2. $NO_x$ storage-reduction activity in the presence of soot

 $NO_X$  adsorption–reduction experiments have been carried out also in the presence of soot in the temperature range 250–350 °C. The results obtained at 350 °C and 250 °C are shown in Fig. 1B and D ( $NO_X$  storage) and Fig. 2B and D ( $NO_X$  reduction).

#### 3.2.1. NO<sub>x</sub> storage

At  $350\,^{\circ}$ C (Fig. 1B) the NO outlet concentration shows a dead time lower than in the absence of soot (Fig. 1A) (i.e.  $90\,\text{s}$  vs.  $210\,\text{s}$ ); then, it increases approaching an asymptotic value of  $880\,\text{ppm}$ . NO is also oxidized to  $NO_2$  whose concentration measured at steady state is near  $100\,\text{ppm}$ .

The amounts of  $NO_x$  stored at steady-state in the presence of soot are near 0.38 mmol/ $g_{cat}$ , i.e. lower if compared to those measured in the absence of soot (0.56 mmol/ $g_{cat}$ ), corresponding to the involvement of 27.5% of K (vs. 40.5% for the soot-free case). Similar effects have been observed at 250 °C (compare Fig. 1D with B) and at the other investigated temperatures (see Fig. 2 and Table 1).

The effect of soot on the  $NO_x$  storage capacity has also been investigated on Ba-based systems [17,30], and similar effects have been pointed out. In fact also for the Ba containing system the presence of soot reduces the  $NO_x$  storage capacity of the catalyst, in line with the results of Pieta et al. [15] and Sullivan et al. [11,12]. According to these authors soot may compete with Ba sites for reaction with  $NO_2$  by offering another reaction route to the desired formation of surface nitrates. In fact the  $NO_2$  concentration at the reactor outlet in the presence of soot is significantly lower than that observed in the absence of soot (compare Fig. 1B and A) possibly due to the participation of  $NO_2$  in the combustion of soot according to the following reaction:

$$2NO_2 + C \rightarrow CO_2 + 2NO \tag{4}$$

Accordingly, in the presence of soot the  $NO/NO_2$  molar ratio is higher than that measured in the case of the soot-free catalyst (near 8.8 vs. 1.72). Note that reaction (4) is a global reaction possibly involving the following two steps:

$$NO_2 + C \rightarrow CO + NO \tag{5}$$

$$CO + 1/2O_2 \rightarrow CO_2$$
 (6)

During our experiments CO formation is not observed, likely because CO is oxidized to  $CO_2$  by  $O_2$  on Pt sites [17].

Notably, by comparing Fig. 1A and B, a more pronounced tail in the NO concentration is observed upon NO shutoff in the presence of soot, indicating that the presence of soot influences the stability of the adsorbed  $NO_X$  species. A significant  $NO_X$  release is apparent also upon oxygen shut off, which on the other hand is negligible over the soot-free catalyst.

In Fig. 1B the trace of the outlet  $CO_2$  concentration is also reported. In the presence of soot, the  $CO_2$  evolution results from two different contributions: (i) the decomposition of surface carbonates upon nitrates formation (reaction (2)); (ii) soot combustion according to the reaction (4). The amounts of  $CO_2$  produced due to soot oxidation (net  $CO_2$  production) have been calculated as previously indicated, and shown in the figure. The soot combustion is

**Table 1** Stored  $NO_x$  up to steady state (NO 1000 ppm,  $O_2$  3% v/v,  $H_2O$  1% v/v,  $CO_2$  0.1% v/v), desorbed  $NO_x$  after  $NO_x$  shutoff (430 s) and desorbed  $NO_x$ /stored  $NO_x$  ratio (%) at different temperatures in the absence and in the presence of soot over Pt-K/ $Al_2O_3$  and Pt-Ba/ $Al_2O_3$  catalysts.

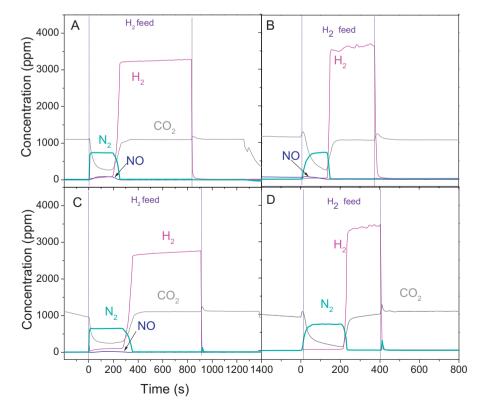
	Without soot			With soot		
	Stored $NO_x$ up to steady state (mmol/g <sub>cat</sub> )	Desorbed NO <sub>x</sub> upon NO shutoff (mmol/g <sub>cat</sub> )	Desorbed NO <sub>x</sub> /stored NO <sub>x</sub> (%)	Stored NO <sub>x</sub> up to steady state (mmol/g <sub>cat</sub> )	Desorbed NO <sub>x</sub> upon NO shutoff (mmol/g <sub>cat</sub> )	Desorbed NO <sub>x</sub> /stored NO <sub>x</sub> (%)
Pt-K/Al <sub>2</sub> O <sub>3</sub>	catalyst					
250°C	0.52	0.03	7	0.36	0.04	11
300 °C	0.62	0.05	8	0.55	0.07	13
320°C	0.61	0.04	7	0.46	0.08	17
350°C	0.56	0.07	12	0.38	0.10	26
Pt-Ba/Al <sub>2</sub> O <sub>3</sub>	catalyst					
200°C	0.28	0.07	25	0.20	0.05	26
300 °C	0.34	0.03	8	0.29	0.04	14
350°C	0.59	0.05	8	0.39	0.05	12

apparent only after NO admission to the reactor, i.e. in the presence of  $O_2$  only, no  $CO_2$  production is observed. This is in line with several literature reports indicating the beneficial effect of NO on soot combustion specifically over noble metal-containing samples [8,16,31,32]. The suggested mechanism is based on the oxidation of NO to  $NO_2$  promoted by Pt;  $NO_2$  rapidly oxidizes soot with formation of  $CO_2$  and NO; NO is then oxidized again by  $O_2$  over Pt and hence it is "recycled". This points out that  $NO_2$  is involved in soot removal. However, a specific role of the stored nitrates is also likely, as pointed out by the observation that the  $NO_x$  release occurring upon NO and  $O_2$  shut-off is higher in the presence than in the absence of soot. This calls for the existence of direct interaction between soot and the stored nitrates which results in the soot combustion as evidenced by the production of  $CO_2$  and NO after NO shutoff according to the following overall stoichiometry (7):

$$3C + 4KNO_3 \rightarrow CO_2 + 4NO + 2K_2CO_3$$
 (7)

Several authors reported that the presence of  $NO_x$  species adsorbed onto the storage material of the LNT catalyst promotes the combustion of soot [6,11,24]. It is suggested that these species decompose increasing the  $NO_2$  concentration in the gas phase, thus favouring the soot oxidation. However recent studies of our group [17,18,33] indicated the direct participation of the surface nitrates in soot oxidation, without their preliminary thermal decomposition, as also pointed out in [13,14,34–36], hence suggesting the involvement of a redox mechanism occurring between nitrates and soot particles.

ICSC experiments in the presence of soot have been performed at other temperatures; the results obtained at 250 °C (taken as example) are shown in Fig. 1D while the quantitative analysis of the results for all the investigated temperatures is reported in Fig. 2 and Table 1. The NO $_{\chi}$  breakthrough increases with temperature but it is always lower than in the absence of soot (i.e. 50 s vs. 90 s at 250 °C). The amounts of NO $_{\chi}$  stored up to steady-state shows a maximum



**Fig. 3.** Reduction phase over Pt-K/Al<sub>2</sub>O<sub>3</sub> in the absence of soot (A:  $350 \,^{\circ}$ C; C:  $250 \,^{\circ}$ C) and in the presence of soot at different temperatures (B:  $350 \,^{\circ}$ C; D:  $250 \,^{\circ}$ C).  $3500 \,^{\circ}$ DPM H<sub>2</sub> in the presence of H<sub>2</sub>O (1% v/v) and CO<sub>2</sub> (0.1% v/v).

at 300 °C and also in this case are always lower than in the absence of soot (Fig. 2 and Table 1).

Also the amounts of desorbed  $NO_x$  after NO shutoff increase with temperature (Table 1) and are always higher than in the absence of soot. This confirms the destabilizing effect of soot on the stored species that is more evident at high temperatures.

Finally, higher NO/NO $_2$  ratios are measured at steady state in the presence of soot as a result of the participation of NO $_2$  in soot oxidation, that becomes significant at temperature higher than 250 °C (a net CO $_2$  formation is observed during the NO adsorption only above 250 °C). Note that by increasing the temperature the participation of the adsorbed NO $_x$  species in the soot combustion increases as well, as pointed out by the net CO $_2$  formation which is observed after NO shut-off.

The data herein presented well parallel those obtained over Pt-Ba/Al<sub>2</sub>O<sub>3</sub> catalyst [17]. However the performances of the Pt- $K/Al_2O_3$  sample in terms of  $NO_x$  storage activity keep higher than those of Ba-based catalyst also in the presence of soot (see Fig. 2 and Table 1). Inspection of Table 1 also shows that, at temperature higher than 300 °C, larger amounts of NO<sub>x</sub> are desorbed over Pt-K/Al<sub>2</sub>O<sub>3</sub> than Pt-Ba/Al<sub>2</sub>O<sub>3</sub>. This is accompanied by a higher production of CO<sub>2</sub> after NO shutoff over Pt-K/Al<sub>2</sub>O<sub>3</sub> than that observed in [17] for Pt-Ba/Al<sub>2</sub>O<sub>3</sub>, indicating a greater contribution of reaction (7) to soot combustion when potassium is present in catalyst formulation instead of barium. In line with the mechanistic proposals suggested above, the greater reactivity of NO<sub>x</sub> stored over K-containing samples can be likely explained on the basis of the higher mobility of nitrates stored on potassium [21,22,37], likely enhancing the soot-catalyst contact [23,38] and hence favouring the soot combustion. As matter of fact, when Ba and K are in tight contact with soot, they exhibit a similar reactivity [32,39], thus confirming that the higher activity of K-based systems even under loose conditions is likely due to the high mobility of the K surface species.

#### 3.2.2. NO<sub>x</sub> reduction

Fig. 3B and D shows the data collected during the rich phase of cycling in the presence of soot at  $350\,^{\circ}\text{C}$  and  $250\,^{\circ}\text{C}$  respectively. The products evolution is similar to that previously described for the regeneration phase in the absence of soot (Fig. 3A and C), being nitrogen the main reduction product; negligible amounts of NO are detected only at high temperature (i.e.  $350\,^{\circ}\text{C}$ ). A comparison with the results obtained in the absence of soot indicates that the presence of soot does not influence significantly the reduction of the stored NO<sub>x</sub> at any temperature.

## 3.3. Effect of soot loading on De-NO $_{x}$ activity and stability of the Pt-K/Al $_{2}O_{3}$ catalyst

The results herein presented point out that the presence of soot affects the catalytic performance of the Pt-K/Al<sub>2</sub>O<sub>3</sub> catalyst by lowering not only the amount but also the stability of the NO<sub>x</sub> adsorbed species. In order to investigate more in details the effect of the soot loading on the catalyst behaviour, and the stability of the Pt-K/Al<sub>2</sub>O<sub>3</sub> upon repeated soot oxidation cycles, a sequence of NO<sub>x</sub> adsorption and reduction cycles (6-7 cycles) has been performed in the presence of soot over a fresh Pt-K/Al<sub>2</sub>O<sub>3</sub> at 350 °C until the complete consumption of soot. The amounts of  $NO_x$  stored during the various lean phases are plotted as a function of the soot loading in Fig. 4 (Run 1, line A-B). After this sequence, the clean catalyst has been mixed again with soot and it has been again cycled under the same experimental conditions until complete soot oxidation for other two times (Run 2, line C-D; Run 3, line E-F of Fig. 4). The storage capacity of the fresh catalyst is also reported for comparison purpose (dashed line). During the first run (line A-B in Fig. 4) with the initial soot loading (near 11% w/w) roughly 0.31 mmol/g<sub>cat</sub> of

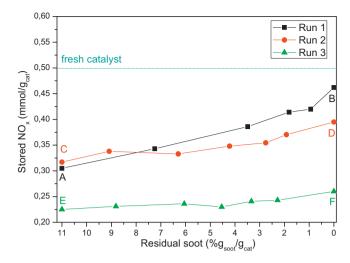


Fig. 4. Stored  $NO_x$  (mmol/ $g_{cat}$ ) as an function of residual soot over Pt- $K/Al_2O_3$  in three subsequent runs.

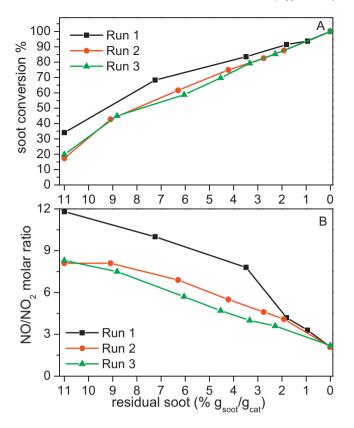
 $NO_x$  have been loaded on the catalyst (point A in Fig. 4). Then, the amounts of  $NO_x$  stored on the catalyst increase upon decreasing the soot loading; roughly 0.46 mmol/ $g_{cat}$  of  $NO_x$  are stored when all the soot has been consumed (point B in Fig. 4). Such amount is very close to that calculated over the fresh catalyst (0.50 mmol/ $g_{cat}$ , dashed line in Fig. 4).

During the second run, the catalyst does not recover the initial  $NO_x$  storage capacity (Run 2, line C–D in Fig. 4) even after complete oxidation of the particulate. The storage capacity remains poor during the third sequence of lean-rich cycles (Run 3, line E–F in Fig. 4).

These data clearly point out that  $NO_x$  storage capacity of LNT Pt-K/Al<sub>2</sub>O<sub>3</sub> catalysts decreases on ageing upon repeated lean-rich cycles. This is in line with the studies of Krishna et al. [8] reporting the decrease of  $NO_x$  storage capacity of Pt/K-Al<sub>2</sub>O<sub>3</sub> catalyst upon ageing under soot oxidation conditions.

The soot oxidation activity of the Pt-K/Al<sub>2</sub>O<sub>3</sub> catalyst has also been evaluated during these runs by calculating the soot conversion during the lean phases and results are shown in Fig. 5A. A reduced soot oxidation activity of the aged Pt-K/Al<sub>2</sub>O<sub>3</sub> catalyst is observed during the second and the third run if compared to the first run. Concerning the NO/NO<sub>2</sub> molar ratio (Fig. 5B), it strictly depends on the soot loading; as expected, the ratio decreases by lowering the amount of soot, since NO2 is not more involved in the soot combustion. However, the NO/NO2 molar ratio calculated over the clean catalysts after the complete removal soot (points in correspondence of residual soot 0%), during all the three runs, is always quite similar to the value calculated for fresh catalyst (near 2.1 vs. 1.72). This indicates that the ageing process seems not to affect the NO oxidizing capacity of the system, occurring at the Pt-sites. Accordingly, the observed decrease in the soot oxidation activity over the aged catalyst could be ascribed to changes in the alkali component and/or losses of the active phase [22,40,41].

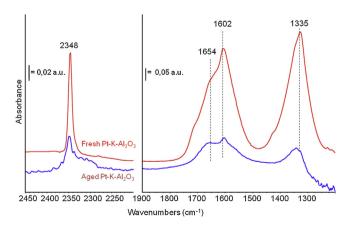
Notably, after the first run the catalyst seems to be stabilized in its oxidation activity. This effect is in line with our previous results obtained with a Pt-free K/Al<sub>2</sub>O<sub>3</sub> catalyst which has been used for repeated soot oxidation cycles at 400 °C [32]. Also in that case, a significant decrease in the combustion activity was noticed passing from the first to the second isothermal cycle but then the catalyst activity becomes stable and reproducible. The reason of such behaviour is still unclear even if modification in surface morphology and composition should be considered as responsible. These aspects were considered by Gross et al. [42] who investigated the stability of potassium/ceria catalysts during successive TPO



**Fig. 5.** Soot conversion (%) (A) and NO/NO<sub>2</sub> molar ratio at NO shutoff (B) as a function of residual soot over Pt-K/Al<sub>2</sub>O<sub>3</sub> during three different runs (1000 ppm NO and 3% O<sub>2</sub> in the presence of H<sub>2</sub>O (1% v/v) and CO<sub>2</sub> (0.1% v/v) at 350  $^{\circ}$ C).

experiments. Based on the FT-IR characterization of both fresh and aged catalysts they observed that, during the ageing, the catalyst reached a steady-state concerning the most relevant species (e.g. carbonates or carbonate-like compounds). These authors considered the sequential formation and decomposition of these compounds during soot combustion, as a prerequisite for a long term catalytic activity. Moreover, they suggested that if these compounds would not decompose, the catalytic surface would be enriched in carbonates composition leading to the catalyst deactivation.

In order to better understand the reason for the observed catalyst loss of activity, the Pt-K/Al<sub>2</sub>O<sub>3</sub> aged sample has been characterized by FT-IR spectroscopy and results compared with the



**Fig. 6.** FT-IR subtraction spectra of fresh and aged Pt- $K/Al_2O_3$  catalyst after outgassing at 350 °C and adsorption of  $CO_2$  at room temperature. The activated surface spectrum has been subtracted.

fresh system. In Fig. 6 the IR spectra obtained after  $CO_2$  adsorption on the fresh and aged  $Pt-K/Al_2O_3$  samples are compared in common scale. The fresh sample spectrum is dominated by a sharp band ay 2348 cm<sup>-1</sup> (molecularly adsorbed  $CO_2$ ) and by two strong bands at 1602 and 1335 cm<sup>-1</sup> due to bridging or bidentate surface carbonate species, resulting from  $CO_2$  reactive adsorption. As shown previously [43,44], these bands are associated to the presence of potassium on the surface and are unaffected by the presence of Pt. The slight complexity of the higher frequency band is likely due to the presence of more slightly different configurations of surface potassium carbonates.

CO<sub>2</sub> adsorption over the spent aged catalyst gives rise to quite similar, but definitely weaker, features, i.e. bands at 1602 and  $1335 \,\mathrm{cm}^{-1}$ , while the component at  $1654 \,\mathrm{cm}^{-1}$  (due to another carbonate species) is very pronounced here. The spectrum observed after CO<sub>2</sub> adsorption on the fresh catalyst is indeed the same observed previously for CO<sub>2</sub> adsorbed on the same catalyst [43] and also on the Pt-free sample [44] while that of the aged sample closely resembles that observed over a sample with a lower K content (3% K/Al<sub>2</sub>O<sub>3</sub> sample, see [44]). This may indicate that the aged sample suffered a partial potassium loss, as pointed out by SEM-EDS analysis showing a small decrease in the K content (6.2% in the fresh sample, 5.7% in the aged catalyst). However the observed effects (loss of the NOx storage and soot oxidation capacity) may also be explained by considering that the availability of K is decreased, e.g. due to interactions with the support and/or with the noble metal whose characteristics are in fact changed on the aged sample (see below). This is in line with the documented intrinsic high activity of K in the soot combustion [39].

To gain further information on the effect of ageing in modifying the behaviour of Pt-K/Al $_2$ O $_3$  catalysts, low temperature CO adsorption has been also performed over the aged catalyst. Fig. 7 shows the spectra of surface species arising after outgassing, upon warming. The band at  $2151\,\mathrm{cm}^{-1}$  is due to CO interacting with hydroxyl groups of the alumina support. In agreement with this assignment, the corresponding OH stretching bands are shifted towards lower frequencies and a negative band can be detected at  $3715\,\mathrm{cm}^{-1}$  in the subtraction spectra (Fig. 7, inset A). The shoulder at  $2180\,\mathrm{cm}^{-1}$  is due to CO linearly coordinated over Al $^3$ + ions, whereas a weak absorption in the range  $2140-2130\,\mathrm{cm}^{-1}$ , has been previously assigned to CO coordinated over exposed K+ over the same fresh catalyst [43]. The low frequency of carbonyl stretching vibrational modes points out that these sites act as very weak Lewis sites.

Spectra reported in Fig. 7 are consistent with those reported by Montanari et al. [43] recorded in the same conditions following adsorption of CO over the fresh Pt-K/Al<sub>2</sub>O<sub>3</sub> catalyst although some differences can be highlighted. In spite of the heavy K-doping, spectra of CO adsorbed over the aged catalyst show residual Lewis sites (exposed Al ions) characterized by the band at 2180 cm<sup>-1</sup>, whereas the frequency of the band due to CO interacting with OHs, close to the frequency of CO adsorbed on pure alumina (2151 vs. 2153 cm<sup>-1</sup>), seems to indicate that the residual OHs at the surface show some acidity consistent with the exposed support. Moreover, the deconvolution of the CO main band (Fig. 7, inset B), following outgassing at -140 °C, clearly evidences three components, at 2156, 2148, and 2140 cm<sup>-1</sup>, the former due to CO H-bound to alumina hydroxyl groups, still detectable after a brief outgassing, and the latter two due to CO coordinated over K<sup>+</sup> sites behaving as Lewis sites. The quality of such K+ sites is not affected by the conditioning (i.e. the frequency reported here are the same discussed in Ref. [43]), but it is clear that these are not anymore the only components in the carbonyl spectra. This effect could be explained again on the basis of a partial loss of available potassium in the aged catalyst, thus exposing support ions and hydroxyl groups, in agreement

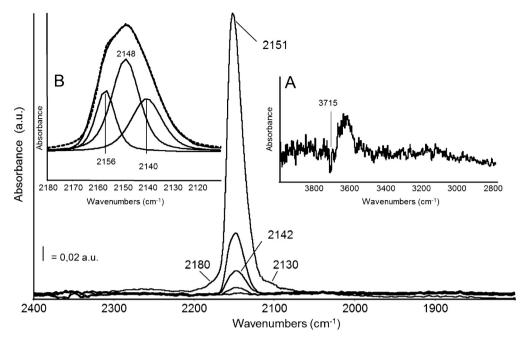


Fig. 7. FT-IR subtraction spectra of the species arising from low temperature CO adsorption over the aged catalyst, outgassed at  $350^{\circ}$ C ( $-140/-80^{\circ}$ C). The activated surface spectrum has been subtracted. Inset A: OH stretching region. Inset B: deconvolution of the spectrum of the species arising from CO adsorption and outgassing at  $-140^{\circ}$ C over the aged catalyst.

with the activity results from ageing tests and from CO<sub>2</sub> reactive adsorption experiments.

Finally, the comparison of aged and fresh Pt-K/Al<sub>2</sub>O<sub>3</sub> catalysts (see Fig. 7 and Ref. [43] respectively) points out some differences concerning also the platinum species. CO adsorption over the fresh catalyst led to the detection of a band at 2075 cm<sup>-1</sup>, due to carbonyls linearly coordinated over Pt metal particles. Moreover, the fresh catalyst showed a quite high oxidizing capability due to residual Pt ions which are able to oxidize CO even at such low temperatures: as a result CO<sub>2</sub> was detected. On the spent catalyst (Fig. 7) the spectral features due to CO adsorbed on Pt metal  $(2100-2000\,\mathrm{cm}^{-1})$  are extremely weak, if any, and  $\mathrm{CO}_2$  was not detected during CO adsorption over the aged catalyst and this effect can be an evidence of modifications of the metal species. On this regard, it may be argued that Pt ions are at least partially covered, or their CO adsorption capacity inhibited, by stronger interaction with K species, as consequence of the above discussed alkali mobility. This however does not lead to appreciable changes in the NO oxidation activity. It is speculated that the Pt sites are more active in the NO oxidation than those present in the fresh catalyst and this may be related to the changes in the K phase resulting in a different interaction with Pt. This point is however not completely understood and deserves further investigations.

#### 4. Conclusions

The data herein presented highlight the catalytic behaviour of DPNR Pt-K/Al $_2$ O $_3$  catalyst in the simultaneous removal of soot and NO $_x$ . It has been found that the presence of soot decreases the storage capacity of the catalytic system at any temperature in the range 250–350 °C. The decrease in the NO $_x$  storage capacity has been related to the competition between soot and K sites towards NO $_2$  that could be involved both in the combustion of soot and/or in the storage process.

Moreover, soot decreases the stability of the  $NO_x$  stored species. In fact, when soot is present, a pronounced tail in the  $NO_x$  concentration is observed upon NO shutoff indicating the decomposition of the adsorbed  $NO_x$ . Besides, a simultaneous production of  $CO_2$ 

is observed. This can be taken as an indication of a direct interaction between soot and stored nitrates leading to soot oxidation, favoured by the high mobility of K-species.

The investigated  $Pt-K/Al_2O_3$  catalyst suffers deactivation upon ageing with repeated  $NO_x$  storage–reduction cycles and soot combustion. In fact the aged catalyst shows a decreased  $NO_x$  storage capacity and also a lower soot oxidation activity. This behaviour has been attributed to a decrease of the availability of the K active species, due to partial loss of K and/or to involvement of the K active species in interactions with alumina and/or Pt.

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